



工程指示 / 要求簡箋(E.I.)

工程指示編號：EI / 9982 / 18

修改版次：-

工程編號：J - 837

工程名稱：觀塘裕民坊

工程項目：Glass Cladding 預留碼 (佛沙場用)

收件人：Maggie

發件人：Eric Liu

日期：29/11/2018

要求提供 / 確認 事項：

- | | | |
|------------------------------------|-------------------------------------|-------------------------------|
| <input type="checkbox"/> 初步鋁料 B.M. | <input type="checkbox"/> 加工拆圖，然後生產 | <input type="checkbox"/> 尺寸表 |
| <input type="checkbox"/> 正式鋁料 B.M. | <input type="checkbox"/> 技術上資料 / 指示 | <input type="checkbox"/> 報價 |
| <input type="checkbox"/> 配件 B.M. | <input type="checkbox"/> 樣辦或貨品說明書 | <input type="checkbox"/> 分判合約 |
| <input type="checkbox"/> 其他：_____ | | |

內容：

請按加工圖生產 Precast glass cladding 用預留碼，送佛沙廠

請留意: 1) 因報關問題，預留碼只能從香港送上中威佛沙廠，不能由大陸送廠

2) T1,3 樓層:由 18/F 開始， T2,5 樓層:由 25/F 開始

3) Precast Glass Cladding 位置: T1E, T3F, T5H

4) 驗焊: Visual: 100%， MPI: 10% (FOR Glass Cladding)

謝謝! EM01, EM02

請在 2018/12/21 前完成上列要求。

張. 安排收貨. 謝

附： 1 頁 B.M.， 1 頁圖登， 2 頁加工圖， 3 頁位置圖

以上項目為:

- 原合約工程包 原合約工程加 / 減賬 新工程報價

原因：-

分發東莞各部門：

- () 生產技術總監 連附件 () 技術部 連附件 () 生產部 連附件 () 機械設計部 連附件
 () 採購部 連附件 () 生產統籌部 連附件
 () 質檢部 連附件 () 會計部 連附件 () 報關組 連附件 () 其他 楊榮輝 連附件

分發香港各部門：

- () 行政部 連附件 () 會計部 連附件 () 統籌部 連附件 () 工程部地盤科文 連附件 火明/祥哥
 () 採購部 連附件 () QS 部 連附件 () 維修部 連附件 () 其他 _____ 連附件

傳遞編號：


HK / 828 / 18

發件人簽署：

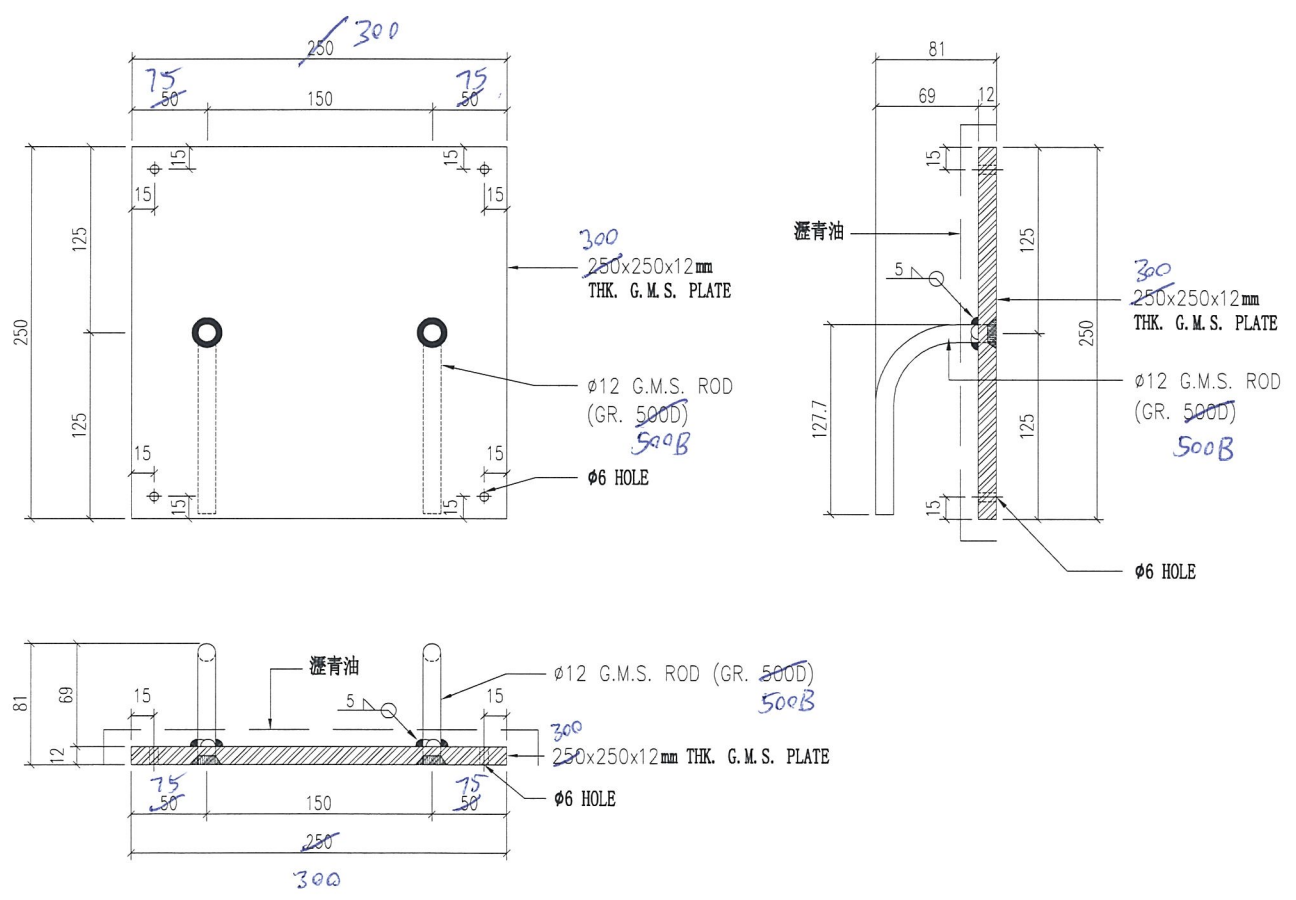
項目經理簽署：

(Handwritten signatures)

2.5 層 = 25 件 / 層
1.3 層 = 18 件 / 層

 美特鋁質有限公司 MIDI Aluminium Fabricator				圖號	數量	位置	樓層	件/層	樓層數
工程號 J-837 地盤 觀塘裕民坊 佛沙場甲 地盤用 單件重量: 6.259KG				GC-EM01	10	T5GC-H	6/F	10	1
					16 136		25/F	8 28	17 2
						27/F	8	1	
						8	28/F~50/F	8	21
						6/F	5	1	
						5	18/F	4	17 8
						27/F	4	1	
						68 32	28/F~52/F	4	23
						27/F	4	1	
						4	28/F~52/F	4	23
						28/F~52/F	4	23	
						92			
小計:					491 316				
後備:					4				
合計:					495 320				


地盤: 安裝鐵角時只燒左右焊



名稱	預留碼拆圖	制圖	羅志光	2018.11.28	修改		
材料	如圖	復核	謝永林		日期		
顏色	熱浸鋅+瀝青油	批准			圖號	GC-EM01	

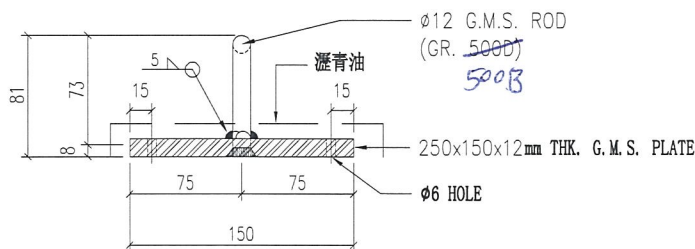
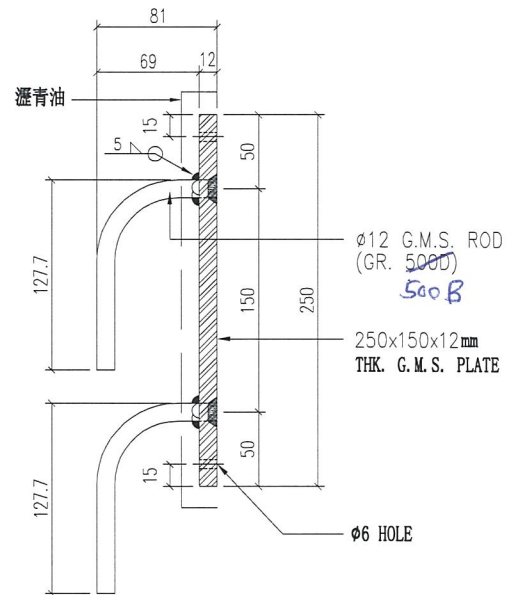
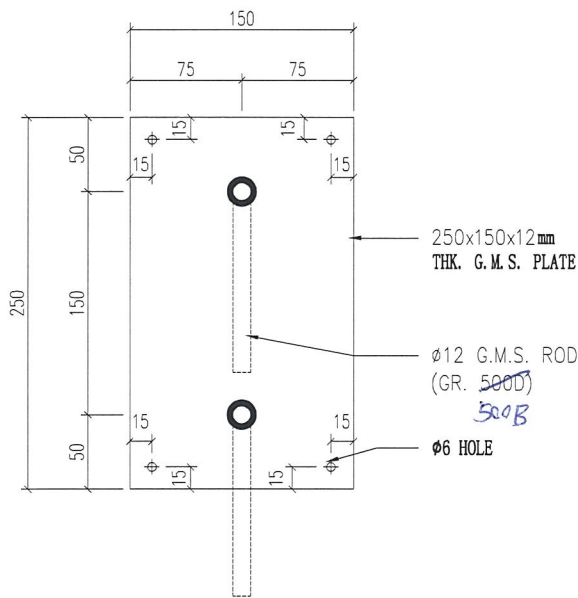
2.5座 = 25/F 以上

1.3座 = 18/F 以上

 美特鋁質有限公司 MIDI Aluminium Fabricator				圖號	數量	位置	樓層	件/層	樓層數		
工程號	J-837	地盤	觀塘裕民坊	GC-EM02	20	T3GC-F	6/F	20	1		
					128 272		18/F	7/F~26/F	16	17 8	
					4		27/F	4	1		
					368		28/F~52/F	16	23		
					5	T1GC-E	6/F	5	1		
					68 32		18/F	7/F~26/F	4	17 8	
					4		27/F	4	1		
					84		28/F~50/F	4	21		
					2	R/F	2	1			
小計：					827	622					
後備：					38						
合計：					830	630					

地盤用
佛沙場用
單件重量：3.904KG

地盤：安裝鐵角時只燒左右焊



名稱	預留碼拆圖	制圖	羅志光	2018. 11. 28	修改		
材料	如圖	復核	謝永林		日期		
顏色	熱浸鋅+瀝青油	批准			圖號	GC-EM02	

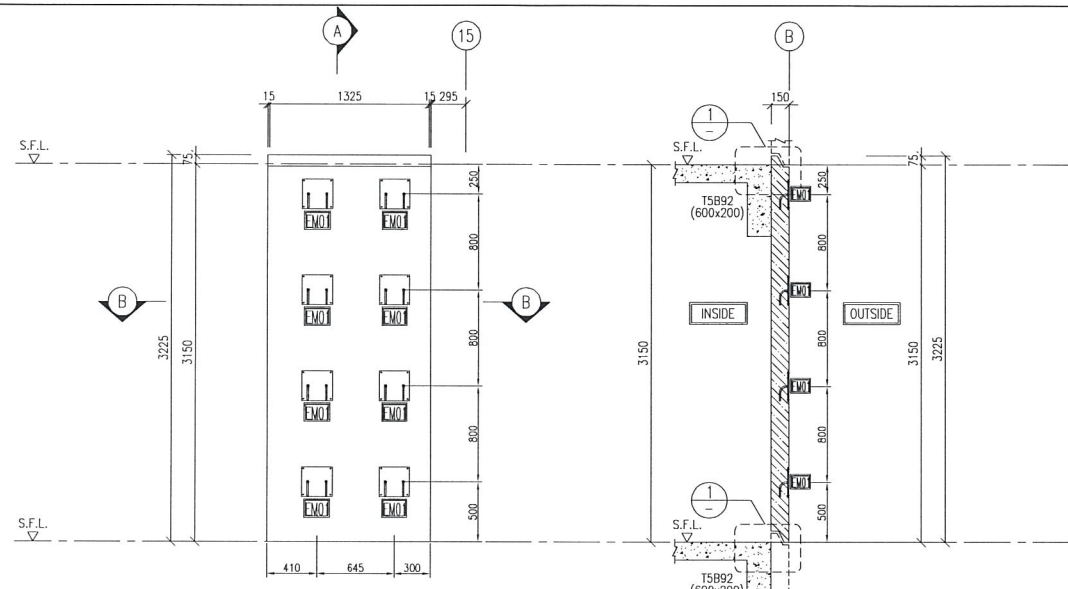
LEVEL	PANEL MARK	QTY.
6/F-26/F, 28/F-50/F	T5PF-H-1	39
WITHOUT 13/F, 14/F, 24/F, 34/F & 44/F		

NOTES:
1. THIS DRAWING SHALL BE READ IN CONJUNCTION WITH THE PRECAST CONCRETE GENERAL ARRANGEMENT (GA) PLAN.

LEGEND:

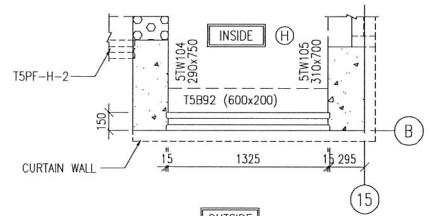
 INSITU CONCRETE
 PRECAST FACADE
 --- ROUGH SURFACE C.J. FACE

T5-H

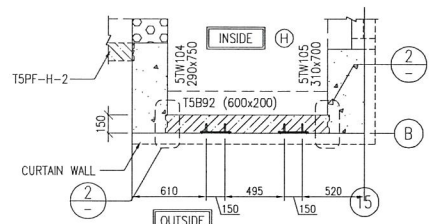


ELEVATION
SCALE 1:40

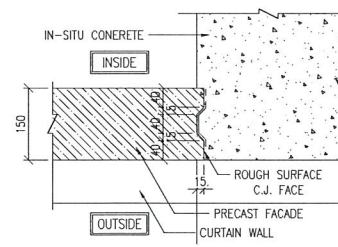
SECTION A-A
SCALE 1:40



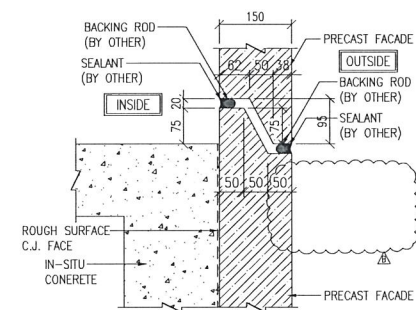
OUTSIDE PLAN
SCALE 1:40



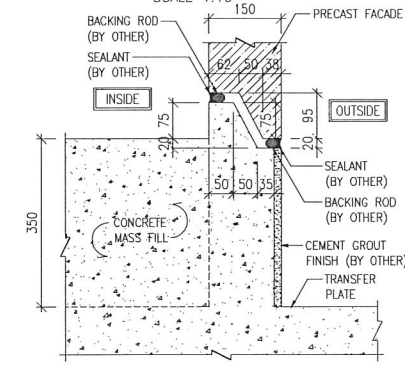
SECTION B-B
SCALE 1:40



DETAIL 2
SCALE 1:10



DETAIL 1
SCALE 1:10



DETAIL 1
(FOR 6/F ONLY) SCALE 1:10

Rev	Amendment	By	Chk.	App.	Date
B	AS CLOURED	CAD	AC	LL	18.05.18
A	AS CLOURED	CAD	AC	LL	16.04.18
-	FIRST ISSUE	CAD	AC	LL	15.02.18

CLIENT:
 ARCHITECT:

STRUCTURE:

MAIN CONTRACTOR:

PRECAST SUPPLIER:

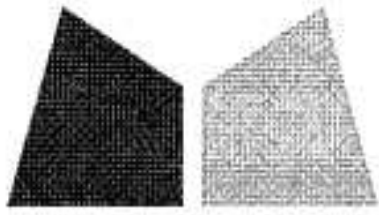
 中國建築預製混凝土有限公司

PROJECT:
 URA KWUN TONG TOWN CENTRE REDEVELOPMENT (AREA 2 & 3) AT NKIL 0514, KWUN TONG, KOWLOON

TITLE:
 SHOP DRAWING
 PRECAST CONCRETE FACADE
 T5PF-H-1 (6/F-26/F, 28/F-50/F ONLY)

Drawn	CAD	Checked	AC	Approved	LL
Scale	1 : 40(A1)	CAD File No.		Date	15.02.2018
First Issued	15.02.2018	Drawing No.	RP/J1802/SD/0192	Rev.	B

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美特鋁質有限公司
MIDI ALUMINIUM FABRICATOR LTD.

PROJECT : URA KWUN TONG TOWN CENTRE
REDEVELOPMENT (AREA 2 & 3)
AT NKIL 6514 KWUN TONG
KOWLOON

TITLE : STRUCTURAL CALCULATION OF
GLASS CLADDING & ALUM FEATURE
Pre-cast Glass Cladding

DATE: 28 NOV 2018

Address Unit 6-8, 1st Floor, Sunray Ind. Centre, 610 Cha Kwo Ling Road Kln.

Tel: 2348 9200

Fax: 2772 7666

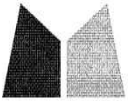
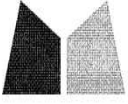
 美特鋁質有限公司 MIDI ALUMINIUM FABRICATOR LTD.	PROJECT:	URA KWUN TONG TOWN CENTRE REDEVELOPMENT (AREA 2 & 3) AT NKIL 6514, KWUN TONG, KOWLOON	
	REPORT DATE:	28/11/2018	REPORT NO:


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 美特鋁質有限公司 MIDI ALUMINIUM FABRICATOR LTD.	PROJECT:	URA KWUN TONG TOWN CENTRE REDEVELOPMENT (AREA 2 & 3) AT NKIL 6514, KWUN TONG, KOWLOON	
	REPORT DATE:	28/11/2018	REPORT NO:

1 Check cast in Embed

1.1 Check Embed EM01 for Central Member

 美特鋁質有限公司 MIDI ALUMINIUM FABRICATOR LTD.	PROJECT:	URA KWUN TONG TOWN CENTRE REDEVELOPMENT (AREA 2 & 3) AT NKIL 6514, KWUN TONG, KOWLOON	
	REPORT DATE:	03/09/2018	REPORT NO: J837-04

D) CHECK EMBED SUPPORT ON PRECAST CONCRETE

LOADS

Support reactions (unfactored) $WL = 3.5 \cdot kN$

$DL = 1.2 \cdot kN$

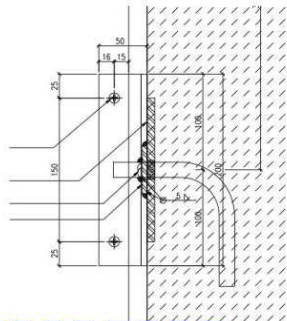
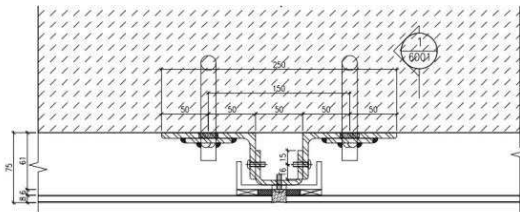
Force on the anchor group (Unfactored)

$R_z := WL = 3.5 \cdot kN$

$R_y := DL = 1.2 \cdot kN$

$e_d := 86mm$

$M_x := DL \cdot e_d = 0.1 \cdot kN \cdot m$



Reaction force on Embed (Unfactored)

$$R_x := 0kN$$

$$R_y = 1.2 \cdot kN$$

$$R_z = 3.5 \cdot kN$$

$$M_x = 0.1 \cdot kN \cdot m$$

$$M_y := 0kN \cdot m$$

$$M_z := 0kN \cdot m$$

Reaction force on Embed (factored)

$$R_{xf} := 0kN$$

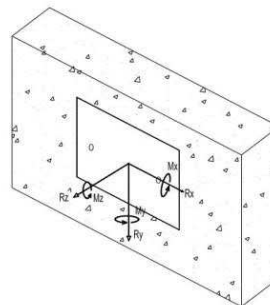
$$R_{yf} := 1.4 \cdot R_y = 1.68 \cdot kN$$

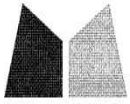
$$R_{zf} := 1.4 \cdot R_z = 4.9 \cdot kN$$

$$M_{xf} := 1.4 \cdot M_x = 0.14 \cdot kN \cdot m$$

$$M_{yf} := 1.4 \cdot M_y = 0 \cdot kN \cdot m$$

$$M_{zf} := 1.4 \cdot M_z = 0 \cdot kN \cdot m$$





美特鋁質有限公司
MIDI ALUMINIUM FABRICATOR LTD.

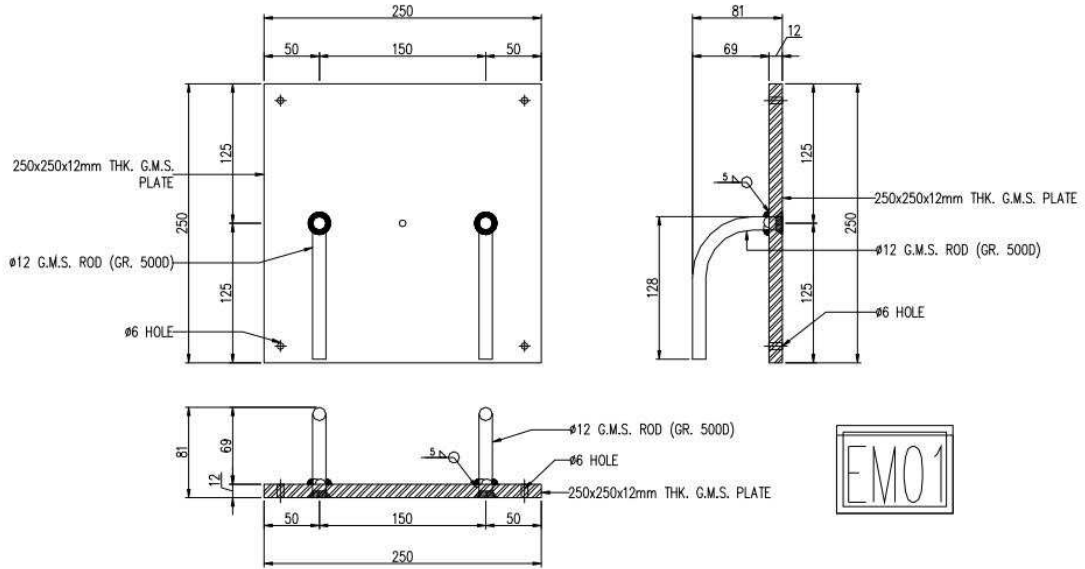
PROJECT:

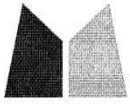
URA KWUN TONG TOWN CENTRE
REDEVELOPMENT (AREA 2 & 3) AT NKIL 6514,
KWUN TONG, KOWLOON

REPORT DATE:

28/11/2018

REPORT NO:





CHECK EMBED EM01 SUPPORT ON PRECAST CONCRETE

LOADS

Support reactions
(unfactored)

$$WL = 3.5 \cdot \text{kN}$$

$$DL = 1.2 \cdot \text{kN}$$

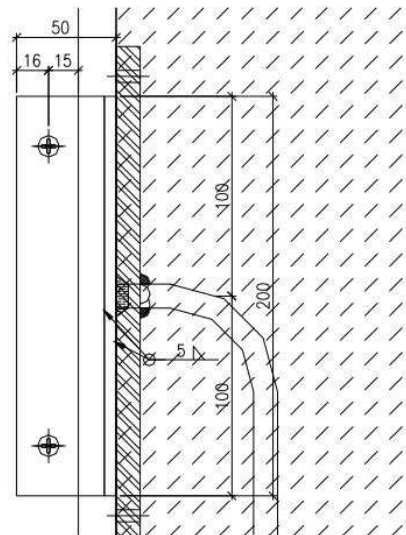
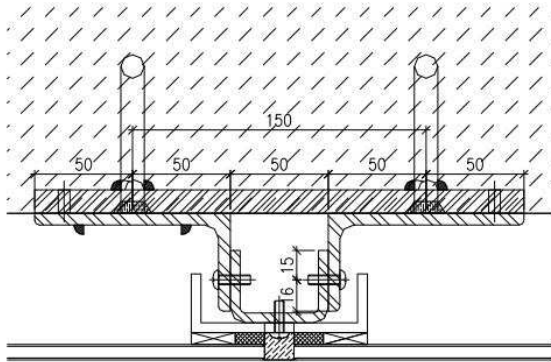
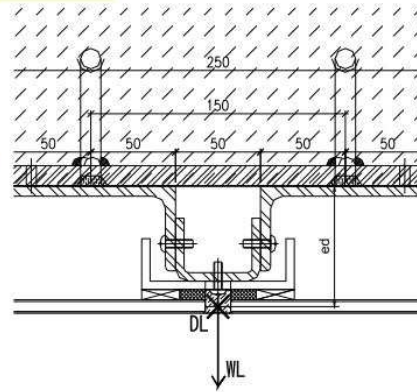
Force on the anchor group
(Unfactored)

$$R_z := WL = 3.5 \cdot \text{kN}$$

$$R_y := DL = 1.2 \cdot \text{kN}$$

$$e_d := 70\text{mm} + 25\text{mm}$$

$$M_x := DL \cdot e_d = 0.11 \cdot \text{kN} \cdot \text{m}$$



Reaction force on Embed (Unfactored)

$$R_x := 0 \text{ kN}$$

$$R_y = 1.2 \cdot \text{kN}$$

$$R_z = 3.5 \cdot \text{kN}$$

$$M_x = 0.11 \cdot \text{kN} \cdot \text{m}$$

$$M_y := 0 \text{ kN} \cdot \text{m}$$

$$M_z := 0 \text{ kN} \cdot \text{m}$$

Reaction force on Embed (factored)

$$R_{xf} := 0 \text{ kN}$$

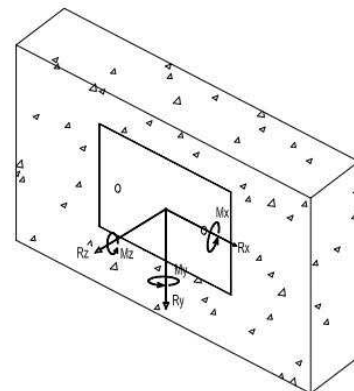
$$R_{yf} := 1.4 \cdot R_y = 1.68 \cdot \text{kN}$$

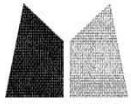
$$R_{zf} := 1.4 \cdot R_z = 4.9 \cdot \text{kN}$$

$$M_{xf} := 1.4 \cdot M_x = 0.16 \cdot \text{kN} \cdot \text{m}$$

$$M_{yf} := 1.4 \cdot M_y = 0 \cdot \text{kN} \cdot \text{m}$$

$$M_{zf} := 1.4 \cdot M_z = 0 \cdot \text{kN} \cdot \text{m}$$





Adopt 2 nos. $\phi 12$ Grade 500B Cast in Bolt

Nos. of bolts per cast-in	$n := 2$
Diameter of bolt	$d_b := 12\text{mm}$
Shear/tensile area of bolt	$A_s := \frac{\pi \cdot d_b^2}{4} = 113.1 \cdot \text{mm}^2$
Anchorage length	$L := 200\text{mm}$

a) Shear force

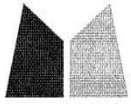
Shear per bolt due to DL	$V_d := \frac{R_{yf}}{n} = 840\text{ N}$
Resultant shear per bolt (factored)	$V := V_d = 840\text{ N}$

b) Check Tension

Direct Tensile force	$T_w := \frac{R_{zf}}{n} = 2.45 \times 10^3\text{ N}$	
Cube strength of concrete at 28 days	$f_{cu} := 35\text{MPa}$	
Bearing strength of concrete	$p_c := 0.4 \cdot f_{cu} = 14 \cdot \text{MPa}$	
Modular ratio = m = modulus of elasticity of steel / modulus of elasticity of concrete		$m_o := 15$
Tensile strength of Grade 8.8 bolt	$p_t := 0.87 \cdot 500\text{MPa} = 435 \cdot \text{MPa}$	

Consider bending moment about x-axis

$d_x := 125\text{mm}$	$d_x = 125 \cdot \text{mm}$	
$dn_x := \left(\frac{p_c \cdot m_o}{p_c \cdot m_o + p_y} \right) \cdot d_x$	$dn_x = 54.12 \cdot \text{mm}$	
$la_x := d_x - \frac{dn_x}{3}$	$la_x = 106.96 \cdot \text{mm}$	
Moment	$M_{xf} = 0.16 \cdot \text{kN} \cdot \text{m}$	
Compressive force due to M_x (factored)	$C_x := \frac{M_{xf}}{2la_x}$	$C_x = 0.75 \cdot \text{kN}$
Tensile force per rod due to M_x (factored)	$T_{mx} := C_x$	$T_{mx} = 0.75 \cdot \text{kN}$
Total tension per bolt (factored)	$T := T_w + T_{mx}$	
	$T = 3.2 \cdot \text{kN}$	



3) Check Grade 500B $\phi 12$ Cast in Bolt

a) Check Shear

Shear per bolt (factored)

$$V = 840 \cdot \text{N}$$

Design shear strength of rod

$$p_s := \frac{0.87 \cdot 500 \text{MPa}}{\sqrt{3}} = 251.15 \cdot \text{MPa}$$

Shear capacity of bolt

$$P_s := p_s \cdot A_s$$

$$P_s = 2.84 \times 10^4 \cdot \text{N} > V = 840 \cdot \text{N} \quad \text{OK}$$

b) Check Tension

Tension per bolt (factored)

$$T = 3.2 \times 10^3 \cdot \text{N}$$

Design tensile strength of rod

$$p_t = 435 \cdot \text{MPa}$$

Tensile capacity of bolt

$$P_t := 0.8 \cdot p_t \cdot A_s$$

$$P_t = 3.94 \times 10^4 \cdot \text{N} > T = 3.2 \times 10^3 \cdot \text{N} \quad \text{OK}$$

c) Check Combined Actions

Combined actions

$$\left(\frac{V}{P_s}\right)^2 + \left(\frac{T}{P_t}\right)^2 = 0.007 < 1.0 \quad \text{OK}$$

4) Check Concrete against Tension from GMS Rods to HKSC 2011

Tension per rod (factored)

$$T = 3.2 \times 10^3 \cdot \text{N}$$

Diameter of rod

$$d_b = 12 \cdot \text{mm}$$

Depth of embedment

$$L = 200 \cdot \text{mm}$$

Design anchorage bond stress per rod

$$f_b := \frac{T}{\pi \cdot d_b \cdot L} \quad \text{to Cl. 9.4.2(a)(i)}$$

$$f_b = 0.42 \cdot \text{MPa}$$

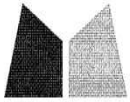
Cube strength of concrete at 28 days

$$f_{cu} = 35 \cdot \text{MPa}$$

Design ultimate anchorage bond stress

$$f_{bu} := 0.5 \cdot \sqrt{\text{MPa}} \cdot (\sqrt{f_{cu}}) \quad \text{to Cl. 9.4.2(a)(i)}$$

$$f_{bu} = 2.96 \cdot \text{MPa} > f_b = 0.42 \cdot \text{MPa} \quad \text{OK}$$



PROJECT:	URA KWUN TONG TOWN CENTRE REDEVELOPMENT (AREA 2 & 3) AT NKIL 6514, KWUN TONG, KOWLOON	
	REPORT DATE:	28/11/2018
REPORT NO:		

5) Check Weld Connection on the Angle Bracket

Resultant force on weld (factored)

$$R_w := \sqrt{V^2 + T^2}$$

$$R_w = 3.3 \times 10^3 \cdot N$$

Thickness of weld

$$t_w := 5 \text{ mm}$$

Diameter of rod

$$d_b = 12 \cdot \text{mm}$$

Weld length

$$L_w := \pi \cdot d_b \quad L_w = 37.7 \cdot \text{mm}$$

Stress from resultant force

$$P_r := \frac{R_w}{L_w}$$

$$P_r = 87.66 \cdot N \cdot \text{mm}^{-1}$$

Design strength of weld

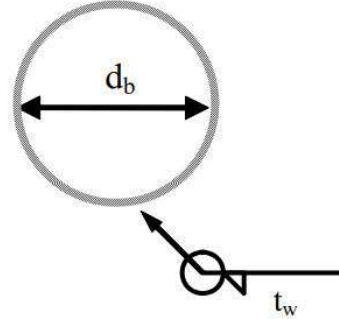
$$p_w := 220 \text{ MPa}$$

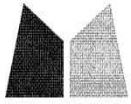
Weld capacity

$$W_c := 0.7 \cdot t_w \cdot p_w$$

$$W_c = 770 \cdot N \cdot \text{mm}^{-1}$$

$$> \quad P_r = 87.66 \cdot N \cdot \text{mm}^{-1} \quad \text{OK}$$





6) CHECK LOCAL BENDING OF GMS ANGLE

Tension per Bolt (factored)

$$T = 3.2 \cdot \text{kN}$$

Thickness of section

$$t := 12 \text{ mm}$$

Eccentricity

$$e := \frac{150 \text{ mm}}{2} = 0.08 \text{ m}$$

Eccentric moment (factored)

$$M_c := T \cdot e$$

$$M_c = 2.4 \times 10^5 \cdot \text{N} \cdot \text{mm}$$

Dia. of bolt

$$d_f := 12 \text{ mm}$$

Edge distance of bolt

$$e_g := 125 \text{ mm}$$

Spacing of anchor

$$s := 150 \text{ mm}$$

Effective breadth
(assume 60 deg
load spread)

$$b_{\text{eff}} := \min\left(e \cdot \tan(60 \text{ deg}), \frac{s}{2}\right) + \min(e \cdot \tan(60 \text{ deg}), e_g)$$

$$b_{\text{eff}} = 200 \cdot \text{mm}$$

Elastic modulus

$$Z := \frac{b_{\text{eff}} \cdot t^2}{6}$$

$$Z = 4800 \cdot \text{mm}^3$$

Plastic modulus

$$S := \frac{b_{\text{eff}} \cdot t^2}{4}$$

$$S = 7200 \cdot \text{mm}^3$$

Design strength for S275 steel

$$p_y := 275 \text{ MPa}$$

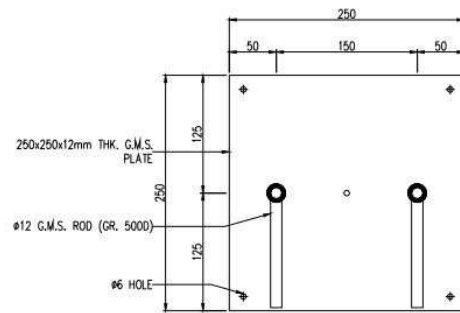
Bending capacity

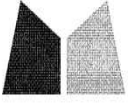
$$M_c := \min(p_y \cdot S, 1.2 p_y \cdot Z)$$

$$M_c = 1.58 \times 10^6 \cdot \text{N} \cdot \text{mm}$$

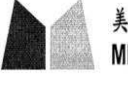
$$> M_c = 2.4 \times 10^5 \cdot \text{N} \cdot \text{mm}$$

OK



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1.2 Check Embed EM02 for Edge Member

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	REPORT DATE:	03/09/2018	REPORT NO:

D) CHECK EMBED SUPPORT ON PRECAST CONCRETE

LOADS

Support reactions (unfactored) $W_L = 1.78\text{-kN}$

$DL = 0.61\text{-kN}$

Force on the anchor group (Unfactored)

$R_x := W_L = 1.78\text{-kN}$

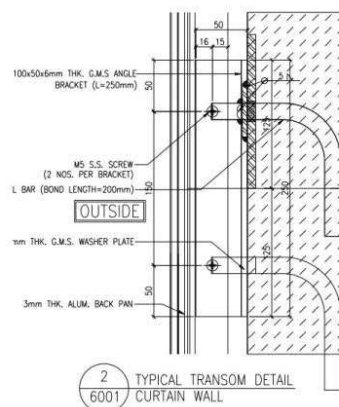
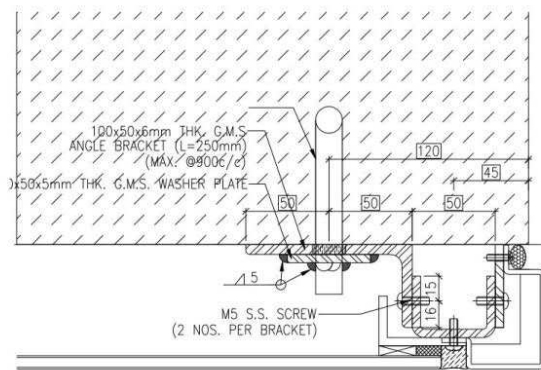
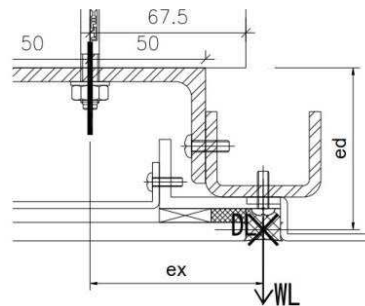
$R_y := DL = 0.61\text{-kN}$

$e_x = 75\text{-mm}$ $e_d = 86\text{mm}$

$M_x := DL \cdot e_d = 0.05\text{-kN}\cdot\text{m}$

$M_y := W_L \cdot e_x = 0.13\text{-kN}\cdot\text{m}$

$M_z := DL \cdot e_x = 0.05\text{-kN}\cdot\text{m}$



Reaction force on Embed (Unfactored)

$R_x := 0\text{kN}$

$R_y = 0.61\text{-kN}$

$R_z = 1.78\text{-kN}$

$M_x = 0.05\text{-kN}\cdot\text{m}$

$M_y = 0.13\text{-kN}\cdot\text{m}$

$M_z = 0.05\text{-kN}\cdot\text{m}$

Reaction force on Embed (factored)

$R_{xf} := 0\text{kN}$

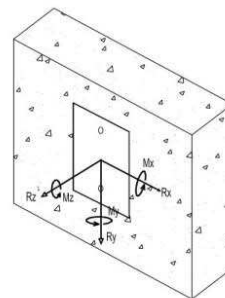
$R_{yf} := 1.4 \cdot R_y = 0.86\text{-kN}$

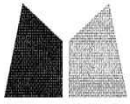
$R_{zf} := 1.4 \cdot R_z = 2.5\text{-kN}$

$M_{xf} := 1.4 \cdot M_x = 0.07\text{-kN}\cdot\text{m}$

$M_{yf} := 1.4 \cdot M_y = 0.19\text{-kN}\cdot\text{m}$

$M_{zf} := 1.4 \cdot M_z = 0.06\text{-kN}\cdot\text{m}$





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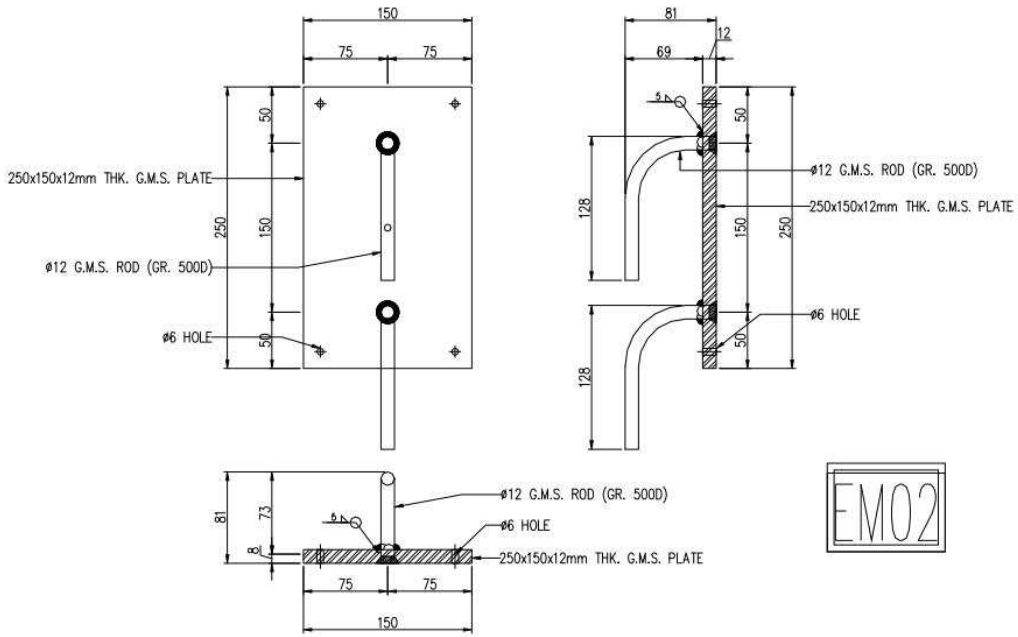
PROJECT:

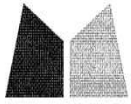
URA KWUN TONG TOWN CENTRE
REDEVELOPMENT (AREA 2 & 3) AT NKIL 6514,
KWUN TONG, KOWLOON

REPORT DATE:

28/11/2018

REPORT NO:





A) CHECK EMBED SUPPORT ON PRECAST CONCRETE

LOADS

Support reactions
(unfactored)

$WL = 1.78 \cdot \text{kN}$

$DL = 0.61 \cdot \text{kN}$

Force on the anchor group
(Unfactored)

$R_z := WL = 1.78 \cdot \text{kN}$

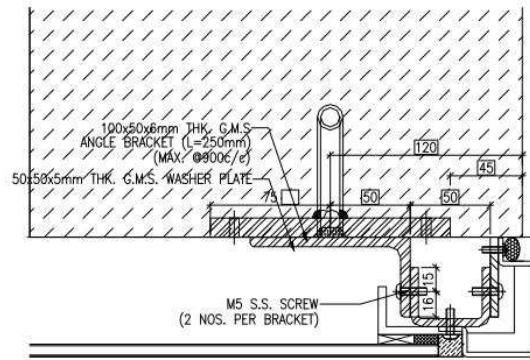
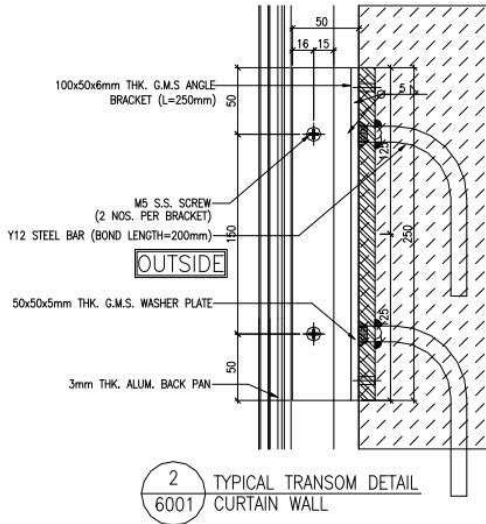
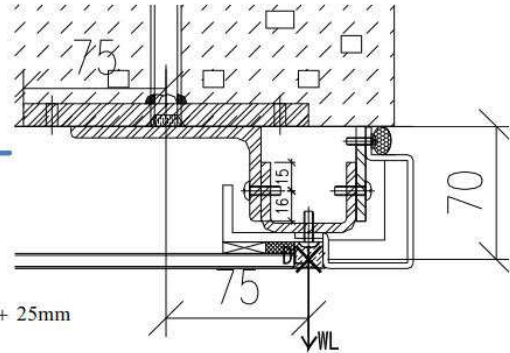
$R_y := DL = 0.61 \cdot \text{kN}$

$e_x := 75\text{mm} + 25\text{mm} \quad e_d := 70\text{mm} + 25\text{mm}$

$M_x := DL \cdot e_d = 0.06 \cdot \text{kN} \cdot \text{m}$

$M_y := WL \cdot e_x = 0.18 \cdot \text{kN} \cdot \text{m}$

$M_z := DL \cdot e_x = 0.06 \cdot \text{kN} \cdot \text{m}$



2
6001 TYPICAL TRANSOM DETAIL
CURTAIN WALL

Reaction force on Embed (Unfactored)

$R_x := 0 \text{ kN}$

$R_y = 0.61 \cdot \text{kN}$

$R_z = 1.78 \cdot \text{kN}$

$M_x = 0.06 \cdot \text{kN} \cdot \text{m}$

$M_y = 0.18 \cdot \text{kN} \cdot \text{m}$

$M_z = 0.06 \cdot \text{kN} \cdot \text{m}$

Reaction force on Embed (factored)

$R_{xf} := 0 \text{ kN}$

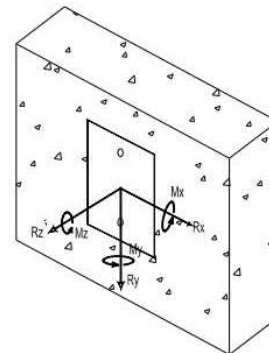
$R_{yf} := 1.4 \cdot R_y = 0.86 \cdot \text{kN}$

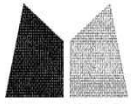
$R_{zf} := 1.4 \cdot R_z = 2.5 \cdot \text{kN}$

$M_{xf} := 1.4 \cdot M_x = 0.08 \cdot \text{kN} \cdot \text{m}$

$M_{yf} := 1.4 \cdot M_y = 0.25 \cdot \text{kN} \cdot \text{m}$

$M_{zf} := 1.4 \cdot M_z = 0.09 \cdot \text{kN} \cdot \text{m}$





Adopt 2 nos. $\phi 12$ Grade 500B Cast in Bolt

Nos. of bolts per cast-in	$n := 2$
Diameter of bolt	$d_b := 12\text{mm}$
Shear/tensile area of bolt	$A_s := \frac{\pi \cdot d_b^2}{4} = 113.1 \cdot \text{mm}^2$
Anchorage length	$L := 200\text{mm}$

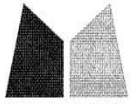
a) Shear force

Shear per bolt due to DL	$V_d := \frac{R_{yf}}{n} = 428.17\text{ N}$
Torsional moment	$M_{zf} = 0.09 \cdot \text{kN} \cdot \text{m}$
Spacing of bolt	$s := 150\text{mm}$
Shear per bolt due to DL	$V_m := \frac{M_{zf}}{s} = 570.89\text{ N}$
Resultant shear per bolt (factored)	$V := \sqrt{V_d^2 + V_m^2} = 713.61\text{ N}$

b) Check Tension

Direct Tensile force	$T_w := \frac{R_{zf}}{n} = 1.25 \times 10^3\text{ N}$	
Cube strength of concrete at 28 days	$f_{cu} := 35\text{MPa}$	
Bearing strength of concrete	$p_c := 0.4 \cdot f_{cu} = 14 \cdot \text{MPa}$	
Modular ratio = m = modulus of elasticity of steel / modulus of elasticity of concrete		$m_o := 15$
Tensile strength of Grade 8.8 bolt	$p_t := 0.87 \cdot 500\text{MPa} = 435 \cdot \text{MPa}$	

Consider bending moment about x-axis



$$d_x := 150\text{mm}$$

$$d_x = 150\text{-mm}$$

$$dn_x := \left(\frac{p_c \cdot m_o}{p_c \cdot m_o + p_y} \right) \cdot d_x$$

$$dn_x = 64.95\text{-mm}$$

$$la_x := d_x - \frac{dn_x}{3}$$

$$la_x = 128.35\text{-mm}$$

Moment

$$M_{xf} = 0.08\text{-kN}\cdot\text{m}$$

Compressive force due to M_x (factored)

$$C_x := \frac{M_{xf}}{la_x}$$

$$C_x = 0.63\text{-kN}$$

Tensile force per rod due to M_x (factored)

$$T_{mx} := C_x$$

$$T_{mx} = 0.63\text{-kN}$$

Consider bending moment about y-axis

$$d_y := 75\text{mm}$$

$$d_y = 75\text{-mm}$$

$$dn_y := \left(\frac{p_c \cdot m_o}{p_c \cdot m_o + p_y} \right) \cdot d_y$$

$$dn_y = 32.47\text{-mm}$$

$$la_y := d_y - \frac{dn_y}{3}$$

$$la_y = 64.18\text{-mm}$$

Moment

$$M_{yf} = 0.25\text{-kN}\cdot\text{m}$$

Compressive force due to M_y (factored)

$$C_y := \frac{M_{yf}}{la_y}$$

$$C_y = 3.89\text{-kN}$$

Tensile force per rod due to M_y (factored)

$$T_{my} := \frac{C_y}{2}$$

$$T_{my} = 1.95\text{-kN}$$

Total tension per bolt (factored)

$$T := T_w + T_{mx} + T_{my}$$

$$T = 3.83\text{-kN}$$

3) Check Grade 500B $\phi 12$ Cast in Bolt

a) Check Shear

Shear per bolt (factored)

$$V = 713.61\text{-N}$$

Design shear strength of rod

$$p_s := \frac{0.87 \cdot 500\text{MPa}}{\sqrt{3}} = 251.15\text{-MPa}$$

Shear capacity of bolt

$$P_s := p_s \cdot A_s$$

$$P_s = 2.84 \times 10^4\text{-N}$$

>

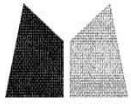
$$V = 713.61\text{-N}$$

OK

b) Check Tension

Tension per bolt (factored)

$$T = 3.83 \times 10^3\text{-N}$$



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Design tensile strength of rod $p_t = 435 \cdot \text{MPa}$
 Tensile capacity of bolt $P_t := 0.8 \cdot p_t \cdot A_s$
 $P_t = 3.94 \times 10^4 \cdot \text{N} > T = 3.83 \times 10^3 \cdot \text{N}$ **OK**

c) Check Combined Actions

Combined actions $\left(\frac{V}{P_s}\right)^2 + \left(\frac{T}{P_t}\right)^2 = 0.01 < 1.0$ **OK**

4) Check Concrete against Tension from GMS Rods to HKSC 2011

Tension per rod (factored) $T = 3.83 \times 10^3 \cdot \text{N}$
 Diameter of rod $d_b = 12 \cdot \text{mm}$
 Depth of embedment $L = 200 \cdot \text{mm}$
 Design anchorage bond stress per rod $f_b := \frac{T}{\pi \cdot d_b \cdot L}$ *to Cl. 9.4.2(a)(i)*
 $f_b = 0.51 \cdot \text{MPa}$
 Cube strength of concrete at 28 days $f_{cu} = 35 \cdot \text{MPa}$
 Design ultimate anchorage bond stress $f_{bu} := 0.5 \cdot \sqrt{\text{MPa}} \cdot (\sqrt{f_{cu}})$ *to Cl. 9.4.2(a)(i)*
 $f_{bu} = 2.96 \cdot \text{MPa} > f_b = 0.51 \cdot \text{MPa}$ **OK**

5) Check Weld Connection on the Angle Bracket

Resultant force on weld (factored) $R_w := \sqrt{V^2 + T^2}$

$R_w = 3.89 \times 10^3 \cdot \text{N}$

Thickness of weld $t_w := 5 \text{ mm}$

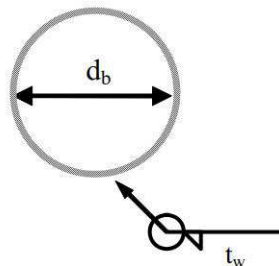
Diameter of rod $d_b = 12 \cdot \text{mm}$

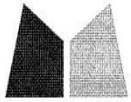
Weld length $L_w := \pi \cdot d_b$
 $L_w = 37.7 \cdot \text{mm}$

Stress from resultant force $P_r := \frac{R_w}{L_w}$
 $P_r = 103.31 \cdot \text{N} \cdot \text{mm}^{-1}$

Design strength of weld $p_w := 220 \text{ MPa}$

Weld capacity $W_c := 0.7 \cdot t_w \cdot p_w$
 $W_c = 770 \cdot \text{N} \cdot \text{mm}^{-1} > P_r = 103.31 \cdot \text{N} \cdot \text{mm}^{-1}$ **OK**





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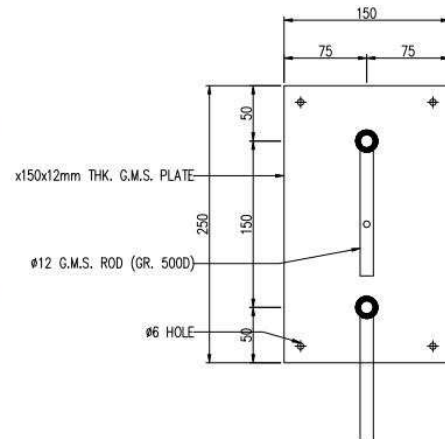
6) CHECK LOCAL BENDING OF GMS ANGLE

Tension per Bolt (factored) $T := 3.83 \cdot \text{kN}$

Thickness of section $t := 12 \text{mm}$

Eccentricity $e := \frac{150 \text{mm}}{2} = 75 \cdot \text{mm}$

Eccentric moment (factored) $M_e := T \cdot e$
 $M_e = 2.87 \times 10^5 \cdot \text{N} \cdot \text{mm}$



Edge distance of bolt $e_g := 75 \text{mm}$

Spacing of anchor $s := 150 \text{mm}$

Effective breadth (assume 60 deg load spread)
 $b_{\text{eff}} := \min\left(e \cdot \tan(60 \text{deg}), \frac{s}{2}\right) + \min(e \cdot \tan(60 \text{deg}), e_g)$
 $b_{\text{eff}} = 150 \cdot \text{mm}$

Elastic modulus $Z := \frac{b_{\text{eff}} \cdot t^2}{6}$ $Z = 3600 \cdot \text{mm}^3$

Plastic modulus $S := \frac{b_{\text{eff}} \cdot t^2}{4}$ $S = 5400 \cdot \text{mm}^3$

Design strength for S275 steel $p_y := 275 \text{MPa}$

Bending capacity $M_c := \min(p_y \cdot S, 1.2 p_y \cdot Z)$

$M_c = 1.19 \times 10^6 \cdot \text{N} \cdot \text{mm} > M_e = 2.87 \times 10^5 \cdot \text{N} \cdot \text{mm}$ **OK**